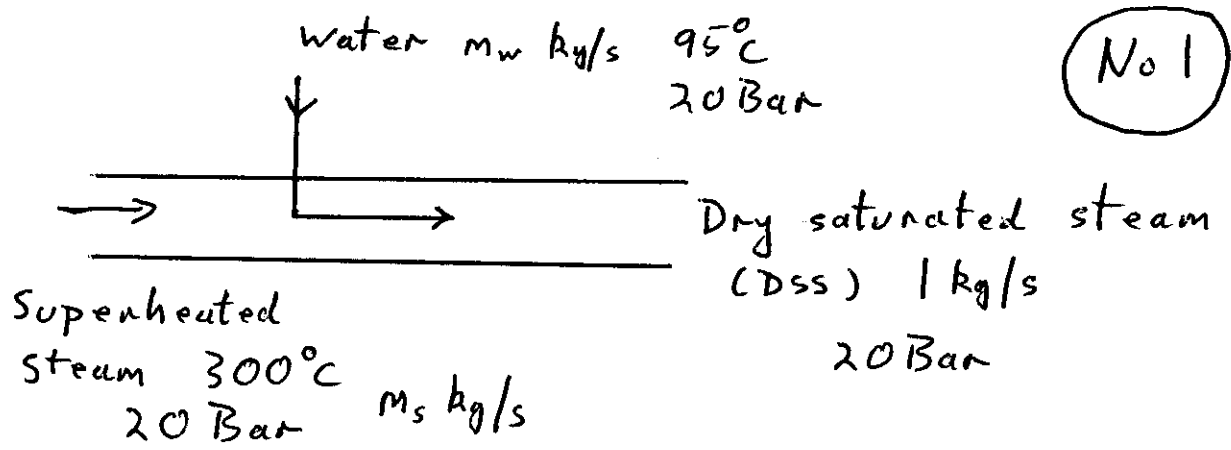


Thermodynamics Tutorial Sheet 3

Worked examples

Answers are given for questions 1, 2 and 3

Questions 4 and 5 are variations on question 3



A 'desuperheater' is a device where water is sprayed into superheated steam, to generate more steam but with less (or zero) superheat.

mass balance: $m_s + m_w = 1$

enthalpy balance: $m_s h_s + m_w h_w = 1 \cdot h_{\text{DSS}}$

At 20 Bar , from superheat tables for steam.
 $h_s = 3025\text{ kJ/kg}$

At 20 Bar , at saturation $h_{\text{DSS}} = 2799\text{ kJ/kg}$

At 20 Bar , at saturation, $h_f = 920\text{ kJ/kg}$
and $T_{\text{sat}} = 215^\circ\text{C}$

$$\begin{aligned} \text{So } h_w &= 920 - 4.18(215 - 95) \\ &= \underline{\underline{418.4\text{ kJ/kg}}} \end{aligned}$$

$$3025 m_s + 418.4 m_w = 2799$$

$$3025 m_s + 418.4(1 - m_s) = 2799$$

$$m_s = 0.913 \text{ kg/s} \quad (3286.8 \text{ kg/hr})$$

$$m_w = 0.087 \text{ kg/s} \quad (313.2 \text{ kg/hr})$$

Under the given superheat conditions:

$$v = 0.1255 \text{ m}^3/\text{kg}$$

Volumetric superheated steam rate

$$= 0.913 \times 0.1255 \quad \frac{\text{kg}}{\text{s}} \times \frac{\text{m}^3}{\text{kg}}$$

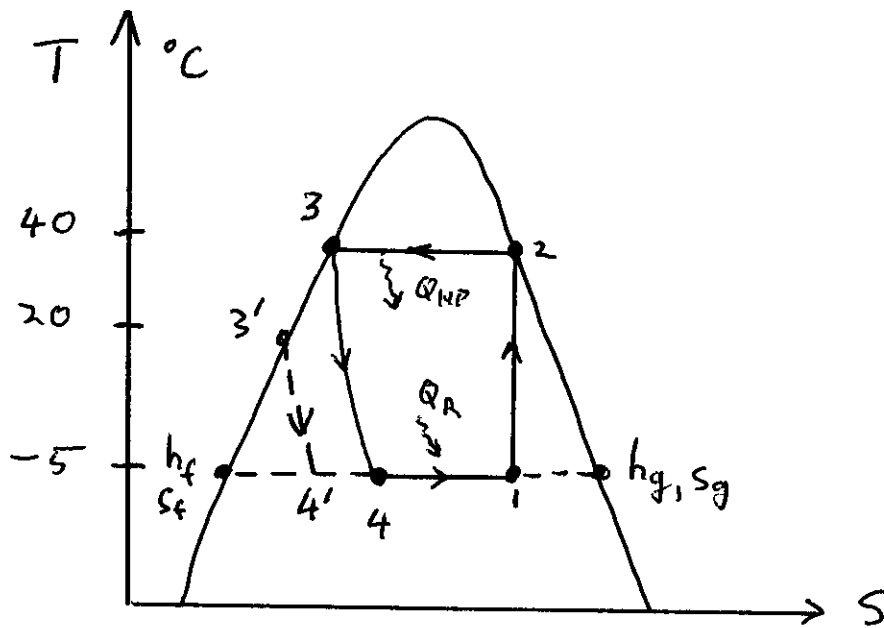
$$= \underline{0.1146 \text{ m}^3/\text{s}}$$

$$= 25 \frac{\text{m}}{\text{s}} \times \frac{\pi D^2}{4} \text{ m}^2$$

$$\Rightarrow D = 0.076 \text{ m}$$

Required pipe diameter $\geq 0.076 \text{ m}$

No 2



$$\text{Refrigeration effect} = h_1 - h_4$$

$$\text{Compressor work (assuming isentropic compression)} = h_2 - h_1$$

$$\text{COP (refrig)} = (h_1 - h_4) / (h_2 - h_1)$$

Dryness fraction at ①:

$$S_2 = S_1$$

$$(1-x)S_f + xS_g = S_1 = S_2$$

$$0.125(1-x) + 0.699x = S_1 = 0.6825 \text{ kJ/kg C}$$

Data from tables
for Freon 12

$$\underline{x = 0.97}$$

Enthalpies:

$$h_1 = (1-x)h_f + xh_g$$

$$= (1-x) \cdot 31.45 + 185.38x$$

$$= \underline{180.8 \text{ kJ/kg}}$$

$$\begin{aligned}h_4 &= h_3 \quad (\text{isenthalpic expansion}) \\ &= 74.6 \text{ kJ/kg} \quad - \text{liquid satn.} \\ &\quad \text{enthalpy at } 40^\circ\text{C}\end{aligned}$$

$$\begin{aligned}h_2 &= 203.2 \text{ kJ/kg} \quad - \text{vapour satn.} \\ &\quad \text{enthalpy at } 40^\circ\text{C}\end{aligned}$$

$$\text{Refrigeration effect} = h_1 - h_4 = 106.2 \frac{\text{kJ}}{\text{kg}}$$

$$\text{COP} = \frac{(h_1 - h_4)}{(h_2 - h_1)} = 4.74$$

With sub cooling to 20°C ,

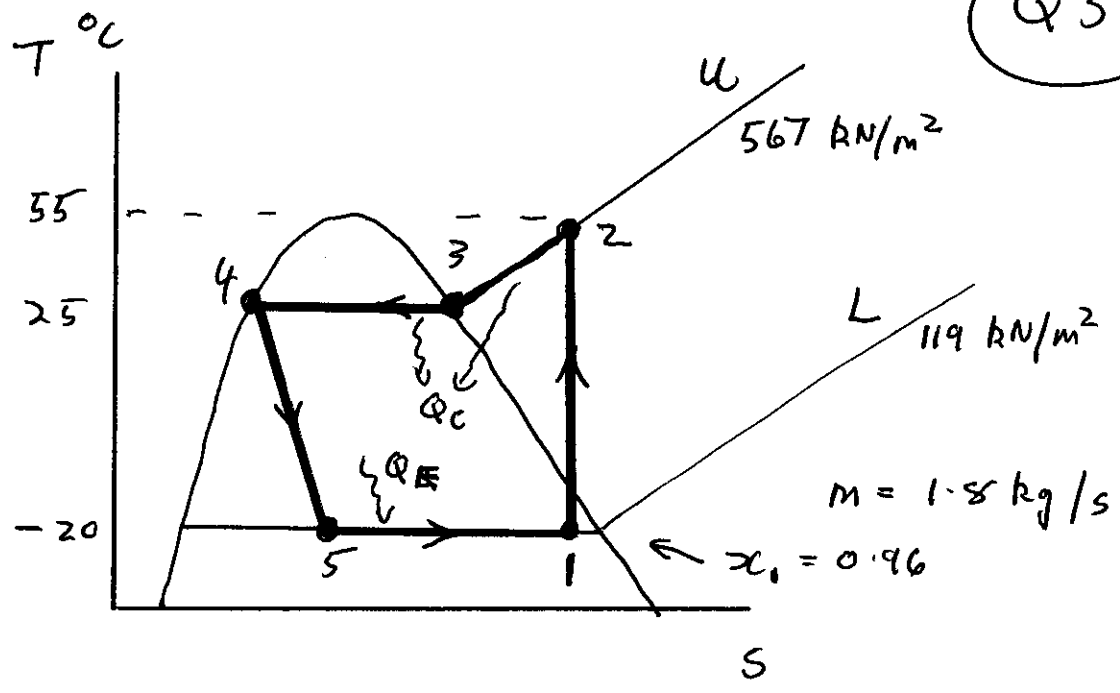
$$h_{3'} = 54.9 \text{ kJ/kg} \quad (\approx \text{liquid satn. at } 20^\circ\text{C})$$

$$\text{So } h_{4'} = 54.9$$

$$\Rightarrow \text{RE} = 125.9 \text{ kJ/kg}$$

$$\text{COP} = 5.62$$

Q3



$$COP = \frac{h_1 - h_5}{h_2 - h_1}$$

$$Q_{COND} = h_2 - h_4$$

$$Q_{EVAP} = h_1 - h_5$$

4 → 5 ISENTHALPIC, 1 → 2 ISENTROPIC

$$h_1 = x h_{g_L} + (1-x) h_{f_L} = 0.96 \times 455.2 + 0.04 \times 30.1 = \underline{438.19 \text{ kJ/kg}}$$

$$h_5 = h_4 = \underline{100.5 \text{ kJ/kg}}$$

$$s_1 = x s_{g_L} + (1-x) s_{f_L} = 0.96 \times 1.803 + 0.04 \times 0.124 = 1.736 \text{ kJ/kg C} = s_2$$

Assume vapour is ideal

$$s_2 - s_3 = C_p \ln \frac{T_2}{T_3} - R \ln \frac{P_2}{P_3}$$
$$= C_p \ln \frac{T_2}{T_3} \quad \text{since } P_2 = P_3$$

$$1.736 - 1.642 = C_p \ln \frac{55 + 273}{25 + 273}$$

$$\underline{C_p = 0.98 \text{ kJ/kg C}}$$

$$h_2 - h_3 = C_p (T_2 - T_3)$$
$$h_2 = 476.8 + 0.98 (55 - 25)$$
$$= \underline{506.2 \text{ kJ/kg}}$$

$$\underline{\underline{COP = h_1 - h_5 / h_2 - h_1 = 4.97}}$$

$$Q_{\text{COND}} = h_2 - h_4 = 405.7 \text{ kJ/kg}$$

$$\text{CONDENSER heat load} = \frac{1.08 \times 405.7}{60}$$

$$= 12.17 \text{ kJ/s}$$

$$= M_w S_w \Delta T_w$$

$$12.17 = \frac{960}{3600} \times 4.187 \times \Delta T_w$$

$$\underline{\underline{\Delta T_w = 10.9^\circ \text{C}}}$$

$$Q_{\text{EVAP}} = h_i - h_s = 337.69 \text{ kJ/kg}$$

$$\begin{aligned} \text{EVAPORATION heat load} &= \frac{1.8}{60} \times 337.69 \\ &= 10.13 \text{ kJ/s} \end{aligned}$$

$$= m_{\text{ice}} \lambda + m_{\text{ice}} \times s_w \times (15 - 0)$$

$$10.13 = m_{\text{ice}} (336 + 4.187 \times 15)$$

$$m_{\text{ice}} = 0.0254 \text{ kg/s}$$

$$= \underline{\underline{91.4 \text{ kg/hr}}}$$